



Designation: D6821 – 20a

# Standard Test Method for Low Temperature Viscosity of Drive Line Lubricants in a Constant Shear Stress Viscometer<sup>1</sup>

This standard is issued under the fixed designation D6821; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope\*

1.1 This test method covers the measurement of the viscosity of drive line lubricants (gear oils, automatic transmission fluids, and so forth) with a constant shear stress viscometer at temperatures from  $-40\text{ }^{\circ}\text{C}$  to  $10\text{ }^{\circ}\text{C}$  after a prescribed preheat and controlled cooling to the final test temperature. The precision is stated for test temperatures from  $-40\text{ }^{\circ}\text{C}$  to  $-26\text{ }^{\circ}\text{C}$ .

1.2 The applicability of this particular test method to petroleum products other than drive line lubricants has not been determined.

1.3 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.3.1 This standard uses the SI based unit of milliPascal second (mPa·s) for viscosity which is equivalent to centiPoise (cP).

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

## 2. Referenced Documents

### 2.1 ASTM Standards:<sup>2</sup>

**D2983 Test Method for Low-Temperature Viscosity of Automatic Transmission Fluids, Hydraulic Fluids, and Lubri-**

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee D02 on Petroleum Products, Liquid Fuels, and Lubricants and is the direct responsibility of Subcommittee D02.07 on Flow Properties.

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<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

**cants using a Rotational Viscometer**

**D3829 Test Method for Predicting the Borderline Pumping Temperature of Engine Oil**

**D4684 Test Method for Determination of Yield Stress and Apparent Viscosity of Engine Oils at Low Temperature**

**D6896 Test Method for Determination of Yield Stress and Apparent Viscosity of Used Engine Oils at Low Temperature**

**D8278 Specification for Digital Contact Thermometers for Test Methods Measuring Flow Properties of Fuels and Lubricants**

**E563 Practice for Preparation and Use of an Ice-Point Bath as a Reference Temperature**

2.2 *ISO Standards:*<sup>3</sup>

**ISO 17025 General Requirements for the Competence of Testing and Calibration Laboratories**

**ISO Guide 34 General Requirements for the Competence of Reference Material Producers**

## 3. Terminology

### 3.1 Definitions:

3.1.1 *apparent viscosity, n*—the determined viscosity obtained by the use of this test method.

3.1.2 *digital contact thermometer (DCT), n*—an electronic device consisting of a digital display and associated temperature sensing probe.

3.1.2.1 *Discussion*—This device consists of a temperature sensor connected to a measuring instrument; this instrument measures the temperature-dependent quantity of the sensor, computes the temperature from the measured quantity, and provides a digital output. This digital output goes to a digital display and/or recording device that may be internal or external to the device.

3.1.2.2 *Discussion*—The devices are often referred to as a “digital thermometers,” however the term includes devices that sense temperature by means other than being in physical contact with the media.

3.1.2.3 *Discussion*—PET is an acronym for portable electronic thermometers, a subset of digital contact thermometers (DCT).

<sup>3</sup> Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

\*A Summary of Changes section appears at the end of this standard

3.1.3 *Newtonian oil or fluid, n*—an oil or fluid that at a given temperature exhibits a constant viscosity at all shear rates or shear stresses.

3.1.4 *non-Newtonian oil or fluid, n*—an oil or fluid that at a given temperature exhibits a viscosity that varies with changing shear stress or shear rate.

3.1.5 *viscosity, n*—the ratio between the applied shear stress and rate of shear which is sometimes called the coefficient of dynamic viscosity and is a measure of the resistance to flow of the liquid.

3.1.5.1 *Discussion*—The SI unit of viscosity is the pascal second [Pa·s]. The submultiple unit is millipascal seconds (mPa·s).

### 3.2 Definitions of Terms Specific to This Standard:

3.2.1 *calibration oils, n*—those oils that establish an instrument's reference framework of apparent viscosity versus speed, from which the apparent viscosities of test oils are determined.

3.2.2 *shear rate, n*—the velocity gradient in fluid flow.

3.2.2.1 *Discussion*—For a Newtonian fluid in a concentric cylinder rotary viscometer in which the shear stress is measured at the inner cylinder surface (such as the apparatus described in 6.1), and ignoring any end effects, the shear rate is given as follows:

$$\dot{\gamma} = \frac{2 \Omega R_s^2}{R_s^2 - R_r^2} \quad (1)$$

$$\dot{\gamma} = \frac{4 \pi R_s^2}{t(R_s^2 - R_r^2)} \quad (2)$$

where:

- $\dot{\gamma}$  = shear rate at the surface of the rotor in reciprocal seconds,  $s^{-1}$ ,
- $\Omega$  = angular velocity, rad/s,
- $R_s$  = stator radius, mm,
- $R_r$  = rotor radius, mm, and
- $t$  = time for one revolution of the rotor, s.

For the specific apparatus being described in 6.1.1,

$$\dot{\gamma} = \frac{33}{t} \quad (3)$$

3.2.3 *shear stress, n*—the motivating force per unit area for fluid flow.

3.2.3.1 *Discussion*—For the rotary viscometer being described in 6.1, the rotor surface is the area under shear or the shear area. For this test method, end effects are not considered.

$$T_r = 9.81 M (R_o + R_l) \times 10^{-6} \quad (4)$$

$$\tau = \frac{T_r}{2 \pi R_r^2 h} \times 10^9 \quad (5)$$

where:

- $T_r$  = torque applied to rotor, N·m,
- $M$  = applied mass, g,
- $R_o$  = radius of the shaft, mm,
- $R_r$  = radius of the string, mm,
- $\tau$  = shear stress at the rotor surface, Pa, and
- $h$  = height of the rotor face, mm.

For the dimensions given in 6.1.1,

$$T_r = 32 M \times 10^{-6} \quad (6)$$

$$\tau = 4.5 M \quad (7)$$

3.2.4 *test oil, n*—any oil for which the apparent viscosity is to be determined by this test method.

3.2.5 *yield stress, n*—the shear stress required to initiate flow.

3.2.5.1 *Discussion*—For Newtonian fluids and some non-Newtonian fluids the yield stress is zero. An oil can have a yield stress that is a function of its low-temperature cooling rate, soak time, and temperature.

## 4. Summary of Test Method

4.1 A drive line fluid is preheated to 50 °C for a specified time and then cooled at a programmed rate (see Table X1.1) to the final test temperature and soaked at the final temperature for a defined period of time. At the completion of the soak time, the viscosity is measured by applying a prescribed torque and measuring rotational speed to determine the apparent viscosity of the sample.

## 5. Significance and Use

5.1 Viscosity of drive line lubricants at low temperature is critical for both gear lubrication and the circulation of the fluid in automatic transmissions. For gear oils (GOs), the issue is whether the fluid characteristics are such that the oil will flow into the channel dug out by the submerged gears as they begin rotating and re-lubricating them as they continue to rotate. For automatic transmission fluids, torque, and tractor fluids the issue is whether the fluid will flow into a pump and through the distribution system rapidly enough for the device to function.

5.2 The low temperature performance of drive line lubricant flow characteristics was originally evaluated by the channel test. In this test, a pan was filled to a specified depth of approximately 2.5 cm and then cooled to test temperature. The test was performed by scraping a channel through the full depth of the fluid and across the length of the pan after it had soaked at test temperature for a specified time. The time it took the fluid to cover the channel was measured and reported. The channel test was replaced by Test Method D2983 in 1971.

5.3 The results of this test procedure correlate with the viscometric measurements obtained in Test Method D2983.<sup>4</sup> The correlation obtained is:

$$V = 0.941 \times V_{D2983} \quad (8)$$

where:

- $V$  = the apparent viscosity measured by this test method, and
- $V_{D2983}$  = the apparent viscosity measured by Test Method D2983.

5.3.1 The equation was obtained by forcing the fit through zero. The coefficient of variation ( $R^2$ ) for this correlation is 0.9948.

<sup>4</sup> SAE Paper 1999-01-3672, "Viscosity of Drive-Line Lubricants by a Special Mini-Rotary Viscometer Technique." Available from Society of Automotive Engineers, 400 Commonwealth Dr., Warrendale, PA 15096-0001.

## 6. Apparatus

6.1 *Mini-Rotary Viscometer*—An apparatus that consists of one or more viscometric cells in a temperature controlled aluminum block. Each cell, when fitted with the specified rotor, becomes a calibrated rotor-stator set. Rotation of the rotor is achieved by an applied load acting through a string wound around the rotor shaft. The top bearing plate is fitted with locking pins for holding the rotors stationary. Time of rotation is measured electronically by a device attached to the timing wheel.

6.1.1 The mini-rotary viscometric cell for this procedure has the following typical dimensions:

Diameter of rotor	15.00 mm ± 0.08 mm
Length of rotor	20.00 mm ± 0.14 mm
Inside diameter of cell	19.07 mm ± 0.08 mm
Radius of shaft	3.18 mm ± 0.13 mm
Radius of string	0.1 mm

6.2 *Weight*—For applying mass. Weights are to be in increments of 2.5 g ± 1 %. A minimum of eight weight segments will be needed for the measurements defined in this test method. One segment will be the weight holder.

6.3 *Temperature Control System*—That will regulate the samples in the cells according to the cooling program described in [Table X1.1](#) and within the tolerances specified in the table.

6.4 *Temperature Measuring Device*—Use either a DCT meeting the requirements described in [6.4.1](#) or liquid-in-glass thermometers described in [6.4.2](#). A calibrated DCT or calibrated low temperature liquid-in-glass thermometer shall be used as the thermometer for temperature measurement below 25 °C independent of the instrument's temperature control, and shall be located in the thermowell.

NOTE 1—The DCT display device and sensor must be correctly paired. Incorrect pairing will result in temperature measurement errors and possibly irreversible damage to the electronics of the display.

6.4.1 *Digital Contact Thermometer*—Use D02-DCT14 listed in Specification [D8278](#). As an alternative to the metal sheathed probe noted in Specification [D8278](#), a glass sheathed DCT probe with a 6 mm O.D. is acceptable provided it meets the other requirements shown for D02-DCT14 in Specification [D8278](#). A DCT display resolution of 0.01 C is preferable. If thermowell ID is larger than the probe OD, then a metallic sleeve must be used to fill the gap between the probe OD and thermowell ID with a length of 58 mm.

6.4.1.1 The DCT calibration drift shall be checked at least annually by either measuring the ice point or against a reference thermometer in a constant temperature bath at the prescribed immersion depth to ensure compliance with [6.4.1](#). With respect to an ice bath, Practice [E563](#) provides guidance on the preparation and use of an ice bath. However, for this use, variance from the specific steps, such as water source, is permitted provided preparation is consistent. The basis for the variance is due to the ice bath reference being used for tracking change in calibration not verification.

NOTE 2—When a DCT's calibration drifts in one direction over several calibration checks, that is, ice point, it may be an indication of deterioration of the DCT.

6.4.2 For liquid-in-glass thermometers, LiG, two are required. One LiG shall be a calibrated 76 mm partial immersion

thermometer with a scale from +5 °C to 1 degree lower than the lowest test temperature in 0.2 °C subdivisions. For test temperatures less than –35 °C, use a liquid-in-glass thermometer with at least a scale range of 2 degrees Celsius in 0.2 °C subdivisions. The low temperature LiG thermometer(s) shall have a report of calibration showing the temperature deviation at each calibrated test temperature. The second LiG thermometer shall be a 76 mm partial immersion thermometer graduated from at least +40 °C to 90 °C in 1 °C subdivisions, which is used to verify the preheat temperature.

6.4.2.1 *Calibration Check*—Verify the low temperature thermometer at least annually against a reference thermometer in a constant temperature bath or in an ice bath. The thermometer is to be inserted to its immersion depth. If using an ice bath, the ice point reading is to be taken within 60 min after the thermometer has been at test temperature for at least 3 min. If the corrected temperature reading deviates from the reference thermometer or the ice point then repeat this calibration check. If the thermometer deviates from the reference value on two successive checks then a full thermometer recalibration is needed.

6.4.2.2 *Recalibration*—A complete recalibration of the liquid-in-glass thermometer, while permitted, is not necessary in order to meet the accuracy ascribed to liquid-in-glass thermometer's design until the thermometers corrected measured temperature deviates from the reference thermometer or ice point by one scale division, or until five years has elapsed since the last full calibration.

6.5 *Supply of Dry Gas*—A supply of dry filtered gas to minimize moisture condensation on the upper portions of the instrument.

6.5.1 For thermoelectric cooled instruments, which use cell caps, the dry gas supply is connected to the housing cover. The supply of dry gas is discontinued when the cover is removed for the measurement phase of the test.

6.6 *Locking Pin*—A device to keep the rotor from turning prematurely and able to stop the rotor at the nearest half revolution by interaction with the rotor crossbar.

## 7. Reagents and Materials

7.1 *Low Cloud-point, Newtonian Oil*, a calibration oil of approximately 60 Pa·s viscosity at –25 °C for calibration of the viscometric cells. The calibration oil shall be obtained from suppliers complying with ISO Guide 34 and ISO 17025 with traceability to a national metrology institute (NMI).

7.2 *Oil Solvent*, commercial heptanes or similar solvent for the test fluids that evaporates without leaving a residue. (**Warning**—Flammable.)

7.3 *Acetone*—A technical grade of acetone is suitable provided it does not leave a residue upon evaporation. (**Warning**—Flammable.)

## 8. Sampling

8.1 A representative sample of test oil free from suspended solid material and water is necessary to obtain valid viscosity measurements. If the sample in its container is received below